

Department of Systems Engineering

George Mason University

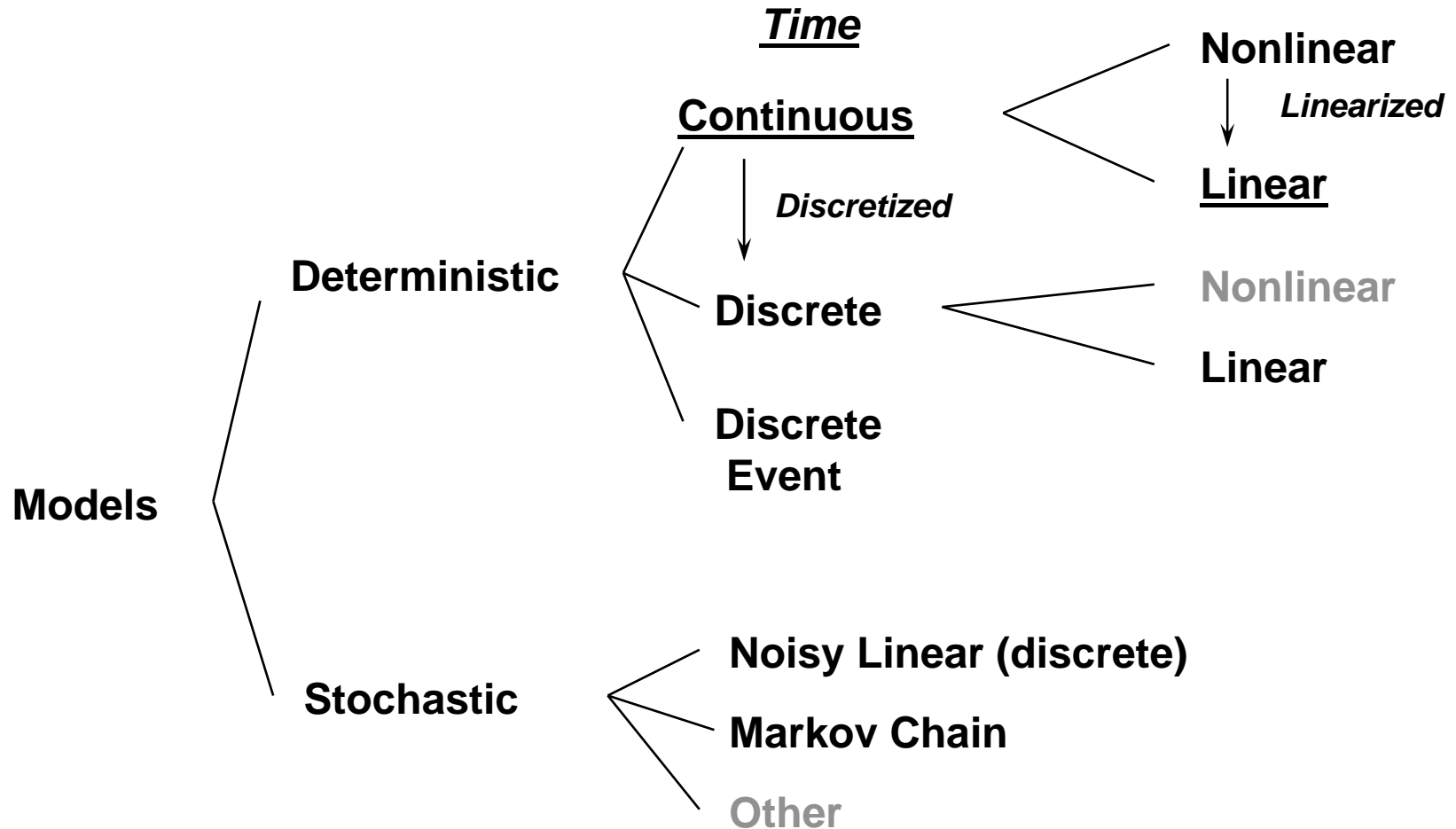
**SYST611: Systems
Methodology and Modeling #3**

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Outline

- **Continuous Linear Systems**
- **Input-Output and State Representations**
- **Stability in Continuous Systems**
- **System Characteristics**

Taxonomy of Models



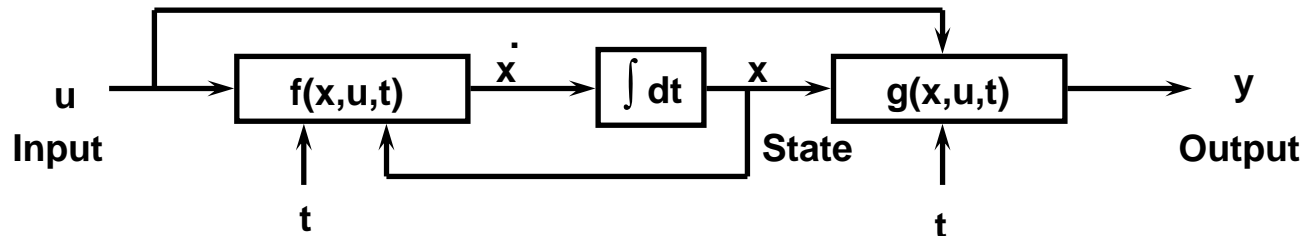
Continuous Time Linear Systems

- **Continuous-Time Systems**

- Ordinary differential equation

$$\dot{x}(t) = f(x, u, t)$$

$$y = g(x, u, t)$$



- **Input-output Representation**

- linear constant coefficient differential equation
(time-invariant)

$$a_n y^{(n)}(t) + a_{n-1} y^{(n-1)}(t) + \dots + a_1 y^{(1)}(t) + a_0 y(t)$$

$$= b_m u^{(m)}(t) + b_{m-1} u^{(m-1)}(t) + \dots + b_1 u^{(1)}(t) + b_0 u(t)$$

Examples

- **Exponential Growth**

$$\frac{dx(t)}{dt} = rx(t) \Rightarrow x(t) = e^{rt} x(0)$$

- **Harmonic Motion**

$$\frac{d^2 y(t)}{dt^2} + \omega^2 y(t) = 0 \Rightarrow y(t) = A \sin \omega t + B \cos \omega t$$

- **Richardson's theory of Arm Race**

$$\dot{x}(t) = ky(t) - \alpha x(t) + g$$

$$\dot{y}(t) = lx(t) - \beta y(t) + h$$

or

$$\begin{bmatrix} \dot{x}(t) \\ \dot{y}(t) \end{bmatrix} = \begin{bmatrix} -\alpha & k \\ l & -\beta \end{bmatrix} \begin{bmatrix} x(t) \\ y(t) \end{bmatrix} + \begin{bmatrix} g \\ h \end{bmatrix}$$

Laplace Transform

For a continuous time function, $y(t)$, defined for $t > 0$

$$Y(s) = L\{y(t)\} = \int_0^{\infty} y(t)e^{-st} dt$$

is called the *Laplace – transform* of $y(t)$

$$\text{Ex : For } y(t) = t^n, L\{t^n\} = \int_0^{\infty} t^n e^{-st} dt = \frac{n!}{s^{n+1}}$$

$$\text{Ex : For } y(t) = e^{-at}, L\{e^{-at}\} = \int_0^{\infty} e^{-at} e^{-st} dt = \frac{1}{s+a}$$

For differential equation,

$$L(y') = \int_0^{\infty} e^{-st} y'(t) dt = e^{-st} y(t) \Big|_0^{\infty} + s \int_0^{\infty} e^{-st} y(t) dt = sL(y) - y(0)$$

In general, for nth order

$$L(y^{(n)}) = s^n L(y) - s^{n-1} y(0) - s^{n-2} y'(0) - \dots - s y^{(n-2)}(0) - y^{(n-1)}(0)$$

Laplace Transform Table

TABLE 4.1

Time Function		Laplace Transform
Unit Impulse	$\delta(t)$	1
Unit Step	$\mathbf{1}(t)$	$\frac{1}{s}$
Unit Ramp	t	$\frac{1}{s^2}$
Polynomial	t^n	$\frac{n!}{s^{n+1}}$
Exponential	e^{-at}	$\frac{1}{s+a}$
Sine Wave	$\sin \omega t$	$\frac{\omega}{s^2 + \omega^2}$
Cosine Wave	$\cos \omega t$	$\frac{s}{s^2 + \omega^2}$
Damped Sine Wave	$e^{-at} \sin \omega t$	$\frac{\omega}{(s+a)^2 + \omega^2}$
Damped Cosine Wave	$e^{-at} \cos \omega t$	$\frac{s+a}{(s+a)^2 + \omega^2}$

Example

Consider the differential equation,

$$y'' - 3y' + 2y = 1$$

with initial conditions: $y(0) = 1$, $y'(0) = 0$

Taking the Laplace transform

$$\Rightarrow [s^2Y(s) - s] - [3sY(s) - 3] + 2Y(s) = \frac{1}{s}$$

$$\Rightarrow (s^2 - 3s + 2)Y(s) = \frac{1}{s} + s - 3 = \frac{s^2 - 3s + 1}{s}$$

Therefore,

$$Y(s) = \frac{s^2 - 3s + 1}{s(s^2 - 3s + 2)} = \frac{1}{2s} + \frac{1}{s-1} - \frac{1}{2(s-2)}$$

$$\Rightarrow y(t) = \frac{1}{2} + e^t - \frac{1}{2}e^{2t}$$

Homogeneous Differential Equations

If the differential equation has no forcing function (i.e. $u(t) = 0$ for all t), then the answer will be a combination of exponentials, e.g.

$$\dot{x}(t) - A(t)x(t) = 0 \text{ or equivalently } \dot{x}(t) = A(t)x(t)$$

then we can use the characteristic function to find the answer.

For example, $\dot{x} - 3x = 0$ has the characteristic function

$$D - 3 = 0, \text{ where } D \equiv \frac{d}{dt}, D^2 \equiv \frac{d^2}{dt^2}, \text{ etc. The roots of the}$$

characteristic equation will be the coefficients of the exponentials,

that is, the solutions will be of the form $x(t) = e^{r_i t}$, where the

terms r_i are the roots of the characteristic equation. In the example

above, the one root is at $D = 3$, so the solution is $x(t) = ce^{3t}$; the

constant c must be determined from initial conditions.

Application: Lanchester Attrition

In 1916 F. W. Lanchester proposed a method for calculating battlefield attrition which has become the standard model of warfare.

While unit A is fighting unit B, unit B is also firing back, decreasing the amount of firepower that A can subsequently direct at B.

$$\frac{dA}{dt} = -b^2 B, \quad \frac{dB}{dt} = -a^2 A$$

Where a is the (dimensionless) coefficient representing the combined firepower effectiveness of unit A on B, and b is the firepower effectiveness of unit B on A.

Differentiate the first equation with respect to time to get a second - order equation :

$$\frac{d^2 A}{dt^2} = -b^2 \frac{dB}{dt}, \text{ substituting the expression for } \frac{dB}{dt} \text{ we get :}$$

$$\frac{d^2 A}{dt^2} = a^2 b^2 A, \text{ a homogeneous differential equation. The characteristic function is}$$

$$D^2 - a^2 b^2 = 0, \therefore D = \pm ab \text{ and } A(t) = c_1 e^{abt} + c_2 e^{-abt}. \text{ At } t = 0, \text{ we have}$$

$$A(0) = c_1 + c_2 \text{ with one solution being } c_1 = c_2 = A_0 / 2 \text{ and } A(t) = \frac{A(0)}{2} (e^{abt} + e^{-abt})$$

Lanchester Attrition ctd.

But wait! There's more...

$$A(t) = \frac{A(0)}{2} (e^{abt} - e^{-abt}) = \cosh(abt).$$

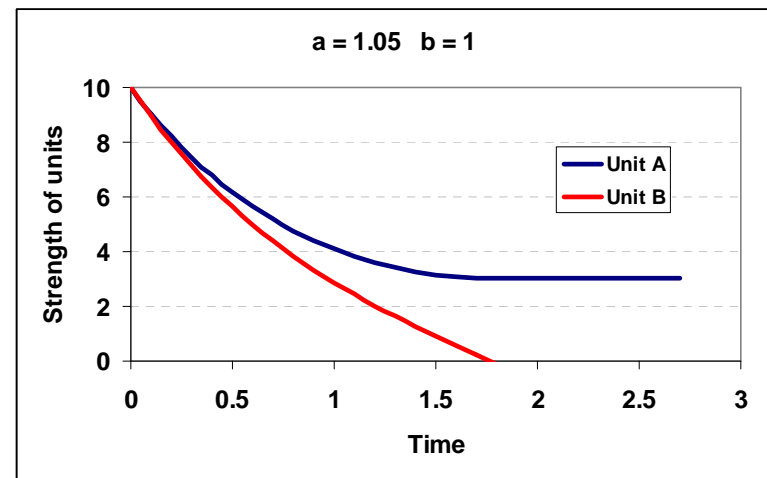
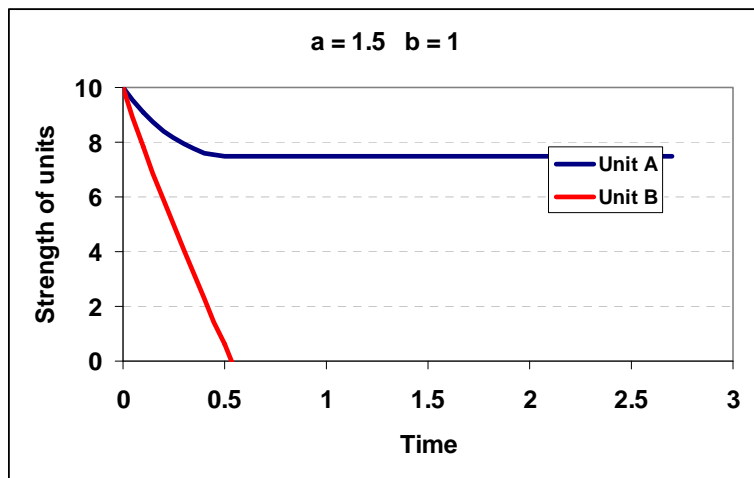
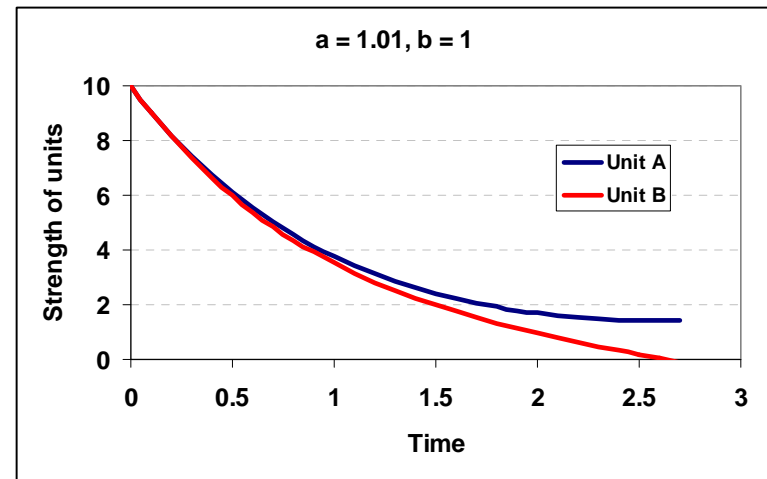
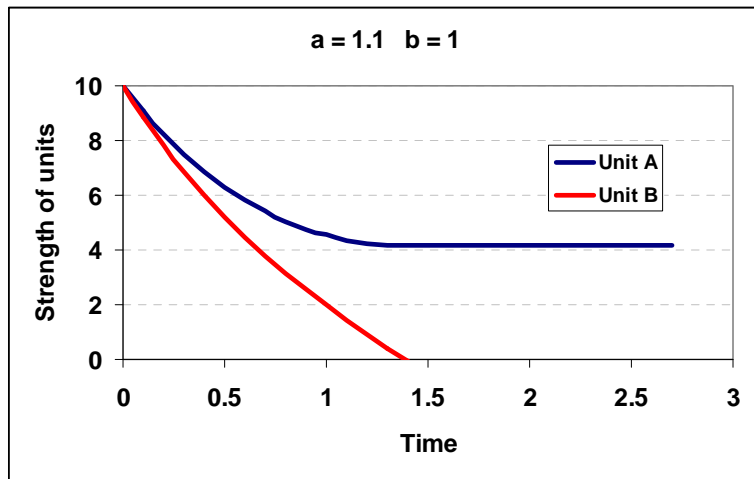
We also know that the derivative $\frac{dA(t)}{dt} = -b^2 B$ from the previous page.

Using that (with much algebra) we get another solution

$$A(t) = \frac{-bB(0)}{2a} e^{abt} + \frac{bB(0)}{2a} e^{-abt} = \frac{-bB(0)}{2a} \sinh(abt) \text{ so the full solution is}$$

$$A(t) = A(0) \cosh(abt) - \frac{B(0)b}{a} \sinh(abt)$$

Lanchester Attrition, concluded



Continuous Linear Systems

Input-Output Representation

- **Transfer Function**

- Apply Laplace transform with zero initial conditions
- Algebraic input-output relationship

$$\sum_{i=0}^n a_i \frac{d^i y}{dt^i} = \sum_{i=0}^m b_i \frac{d^i u}{dt^i} \Rightarrow \left(\sum_{i=0}^n a_i s^i \right) Y(s) = \left(\sum_{i=0}^m b_i s^i \right) U(s)$$

$$\Rightarrow Y(s) = H(s)U(s), \text{ where } H(s) = \frac{\left(\sum_{i=0}^m b_i s^i \right)}{\left(\sum_{i=0}^n a_i s^i \right)} \text{ is called the Transfer Function}$$

and $\left(\sum_{i=0}^n a_i s^i \right)$ is called the *Characteristic Equation*

$H(s)$ is also the *Laplace* transform of the system's **Impulse Response** $y_s(t)$

where $Y(s) = L\{y(t)\} = \int_0^{\infty} y(t)e^{-st} dt$ is the *Laplace – transform* of $y(t)$

Continuous Linear Systems

State Variable Representation

Consider nth - order single input system $\sum_{i=0}^n a_i \frac{d^i y}{dt^i} = u(t)$

$$\left\{ \begin{array}{l} x_1(t) = y(t) \\ \dot{x}_1(t) = x_2(t) = \dot{y}(t) \\ \dot{x}_2(t) = x_3(t) = \ddot{y}(t) \\ \dots \\ \dot{x}_{n-1}(t) = x_n(t) = y^{(n-1)}(t) \\ \dot{x}_n(t) = y^{(n)}(t) = -\frac{1}{a_n} \left[\sum_{i=0}^{n-1} a_i y^{(i)}(t) \right] + \frac{1}{a_n} u(t) = -\frac{1}{a_n} \left[\sum_{i=0}^{n-1} a_i x_{i+1}(t) \right] + \frac{1}{a_n} u(t) \end{array} \right.$$

$$\begin{bmatrix} \dot{x}_1(t) \\ \dot{x}_2(t) \\ \vdots \\ \dot{x}_n(t) \end{bmatrix} = \begin{bmatrix} 0 & 1 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & 0 \\ \vdots & \vdots & \vdots & \ddots & \vdots \\ -a_0/a_n & -a_1/a_n & -a_2/a_n & \dots & -a_{n-1}/a_n \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \\ \vdots \\ x_n(t) \end{bmatrix} + \begin{bmatrix} 0 \\ 0 \\ \vdots \\ 1/a_n \end{bmatrix} u(t)$$

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{b}u(t), \text{ Note : } \det[\mathbf{A} - \lambda I] = \left(\sum_{i=0}^n a_i \lambda^i \right)$$

Examples

Ex1: Harmonic Motion,

$$y'' + \omega^2 y = 0$$

Characteristic equation :

$$\lambda^2 + \omega^2 = 0 \Rightarrow \lambda = \pm i\omega \Rightarrow y(t) = c_1 e^{i\omega t} + c_2 e^{-i\omega t}$$

For real - valued solution, $y(t) = A \sin \omega t + B \cos \omega t$

In state - variable form, let $x_1 = y, x_2 = \dot{x}_1$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\omega^2 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = A \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \Rightarrow \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = e^{At} \begin{bmatrix} x_1(0) \\ x_2(0) \end{bmatrix}$$

$$\text{But } e^{At} = \begin{bmatrix} \cos \omega t & \sin \omega t / \omega \\ -\omega \sin \omega t & \cos \omega t \end{bmatrix}$$

Ex2: $\ddot{y} + \dot{y} + y = u$ let $x_1 = y, x_2 = \dot{y}$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -1 & -1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \end{bmatrix} u$$

I/O to State Representation

In general, consider nth - order system
$$\sum_{i=0}^n a_i \frac{d^i y}{dt^n} = \sum_{j=0}^m b_j \frac{d^j u}{dt^j}$$

The corresponding state representation is:

$$\dot{X} = AX + Bu, \quad y = CX$$

$$A = \begin{bmatrix} -a_{n-1}/a_n & 1 & 0 & \cdots & 0 \\ \vdots & 0 & 1 & \cdots & 0 \\ -a_1/a_n & \vdots & \vdots & \ddots & 1 \\ -a_0/a_n & 0 & 0 & \cdots & 0 \end{bmatrix}, B = \begin{bmatrix} b_{n-1}/a_n \\ \vdots \\ b_1/a_n \\ b_0/a_n \end{bmatrix}$$

$$C = [1 \quad 0 \quad \cdots \quad 0]$$

This is called the “observable canonical form” and matrix A is called the companion matrix

State to I/O Representation

Given the state representation:

$$\dot{X} = AX + Bu, \quad y = CX$$

Use the "differentiation operator" $D \equiv \frac{d}{dt}$

$$\Rightarrow DX = AX + Bu$$

$$(DI - A)X = Bu$$

$$X = (DI - A)^{-1}Bu \Rightarrow y = C(DI - A)^{-1}Bu = H(D)u$$

$$y = \frac{\sum_{i=0}^m b_i D^i}{\sum_{i=0}^n a_i D^i} u \Rightarrow \left(\sum_{i=0}^n a_i D^i \right) y = \left(\sum_{i=0}^m b_i D^i \right) u$$

$$\Rightarrow \sum_{i=0}^n a_i \frac{d^i y}{dt^i} = \sum_{j=0}^m b_j \frac{d^j u}{dt^j}$$

Example – State to I/O

Given the state representation:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 2 & 3 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \\ 0 \end{bmatrix} u, \quad y = \begin{bmatrix} 4 & 1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$y = C(DI - A)^{-1}Bu = \begin{bmatrix} 4 & 1 \end{bmatrix} \begin{bmatrix} D-1 & 0 \\ -2 & D-3 \end{bmatrix}^{-1} \begin{bmatrix} 1 \\ 0 \end{bmatrix} u = \frac{4D-10}{D^2-4D+3} u$$

$$\Rightarrow (D^2 - 4D + 3)y = (4D - 10)u$$

$$\Rightarrow \ddot{y} - 4\dot{y} + 3y = 4\dot{u} - 10u$$

Convert back to state representation with "observable canonical form"

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 4 & 1 \\ -3 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 4 \\ -10 \end{bmatrix} u, \quad y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

Example – Verification

Given the state representation:

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 4 & 1 \\ -3 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 4 \\ -10 \end{bmatrix} u, \quad y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix}$$

$$y = C(DI - A)^{-1}Bu = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} D-4 & -1 \\ 3 & D \end{bmatrix}^{-1} \begin{bmatrix} 4 \\ -10 \end{bmatrix} u = \frac{4D-10}{D^2-4D+3}u$$

$$\Rightarrow (D^2 - 4D + 3)y = (4D - 10)u$$

$$\Rightarrow \ddot{y} - 4\dot{y} + 3y = 4\dot{u} - 10u$$

\Rightarrow Same I/O representation with two different
state space representations

Solution of Continuous Linear Systems

$$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}u(t)$$

General solution = $\mathbf{x}(t) = \mathbf{x}_h(t) + \mathbf{x}_p(t)$

Homogeneous solution : unforced equation with initial condition

$$\dot{\mathbf{x}}_h(t) = \mathbf{A}\mathbf{x}_h(t); \mathbf{x}_h(0) = \mathbf{x}_0$$

icbest $\mathbf{x}_h(t) = e^{\mathbf{A}t} \mathbf{x}_0$ (Free Response)

Particular solution : forced equation with zero initial condition

$$\dot{\mathbf{x}}_p(t) = \mathbf{A}\mathbf{x}_p(t) + \mathbf{B}u(t); \mathbf{x}_p(0) = 0$$

Let $\mathbf{w}(t) = e^{-\mathbf{A}t} \mathbf{x}_p(t)$, then $\dot{\mathbf{w}}(t) = -\mathbf{A}e^{-\mathbf{A}t} \mathbf{x}_p(t) + e^{-\mathbf{A}t} \dot{\mathbf{x}}_p(t) = e^{-\mathbf{A}t} \mathbf{B}u(t)$

i.e., $\mathbf{w}(t) = \int_0^t e^{-\mathbf{A}\tau} \mathbf{B}u(\tau) d\tau \Rightarrow \mathbf{x}_p(t) = \int_0^t e^{\mathbf{A}(t-\tau)} \mathbf{B}u(\tau) d\tau$ (Forced Response)

$$\mathbf{x}(t) = \mathbf{x}_h(t) + \mathbf{x}_p(t) = e^{\mathbf{A}t} \mathbf{x}_0 + \int_0^t e^{\mathbf{A}(t-\tau)} \mathbf{B}u(\tau) d\tau \quad (\text{Total Response})$$

Stability

- **Stable**: A system is *stable* if every solution $x(t)$ corresponding to $u(t)=0$ is bounded for all t
 - A stable system remains at rest unless excited by external forces and returns to rest after all excitations are removed

$$\|x_h(t)\| < B, \quad \forall t$$

- **Asymptotically Stable**: If a system is stable and $x(t)$ tends to 0 when $t \rightarrow \infty$
- **Marginally Stable**: If a system is stable and not asymptotically stable
- **Unstable**: If a system is not stable

Stability Criteria

- **Stable Systems:**

$$\mathbf{x}_h(t) = e^{\mathbf{A}t} \mathbf{x}(0) < B, \forall t$$

$$\text{But } e^{\mathbf{A}t} = T e^{\Lambda t} T^{-1} \text{ and } e^{\Lambda t} = \text{diag}[e^{\lambda_i(\mathbf{A})t}]$$

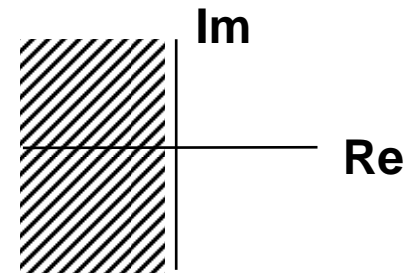
$$\text{In general : } e^{\lambda t} = e^{\lambda_R t} e^{j\lambda_I t} = e^{\lambda_R t} [\cos(\lambda_I t) + j \sin(\lambda_I t)]$$

- **Criteria:** $\text{Re}(\lambda_i) \leq 0, \forall i \rightarrow \text{Stable}$

$$\text{Re}(\lambda_i) < 0, \forall i \rightarrow \text{Asymptotically Stable}$$

where λ_i are solutions of the characteristic equation

$$p(\lambda) = \det[\mathbf{A} - \lambda I] = a_n \lambda^n + a_{n-1} \lambda^{n-1} + \dots + a_1 \lambda + a_0 = 0$$



- **Stability Tests:**

- Routh test (BD p. 93)
- Hurwitz test (JD p.116)

Routh Stability Test

$$a_n s^n + a_{n-1} s^{n-1} + \dots + a_1 s + a_0 = 0$$

Routh table

s^n	a_n	a_{n-2}	a_{n-4}	\dots		
s^{n-1}	a_{n-1}	a_{n-3}	a_{n-5}	\dots	$b_1 = \frac{a_{n-1}a_{n-2} - a_n a_{n-3}}{a_{n-1}}$	$b_2 = \frac{a_{n-1}a_{n-4} - a_n a_{n-5}}{a_{n-1}}$ etc.
·	b_1	b_2	b_3	\dots		
·	c_1	c_2	c_3	\dots	$c_1 = \frac{b_1 a_{n-3} - a_{n-1} b_2}{b_1}$	$c_2 = \frac{b_1 a_{n-5} - a_{n-1} b_3}{b_1}$ etc.
·	\dots	\dots	\dots	\dots		

The Routh Criterion: All the roots of the characteristic equation have negative real parts if and only if the elements of the first column of the **Routh table** have the same sign.

Example I

$$H(s) = s^3 + 6s^2 + 12s + 8 = 0$$

Routh Table

s^3	1	12	0
s^2	6	8	0
s^1	$\frac{64}{6}$	0	
s^0	8		

MATLAB test

```
lambda = roots([1 6 12 8])
```

```
lambda =
```

```
-2.0000
```

```
-2.0000 + 0.0000i
```

```
-2.0000 - 0.0000i
```

No sign change in the first column
-> Stable system

Example - II



$$\begin{bmatrix} \dot{q} \\ \dot{a} \end{bmatrix} = \begin{bmatrix} m_q & m_a \\ 1 & k_a \end{bmatrix} \begin{bmatrix} q \\ a \end{bmatrix} + \begin{bmatrix} m_e & m_f \\ k_e & k_f \end{bmatrix} \begin{bmatrix} e(t) \\ f(t) \end{bmatrix}$$

q : pitch rate (angular velocity)

a : angle of attack

e, f : elevator and flap deflections

$$p(\lambda) = \det \begin{bmatrix} m_q - \lambda & m_a \\ 1 & k_a - \lambda \end{bmatrix} = \lambda^2 - (m_q + k_a)\lambda + (m_q k_a - m_a)$$

Routh table

s^n	1	$m_q k_a - m_a$
s^{n-1}	$-(m_q + k_a)$	0
\cdot	$m_q k_a - m_a$	
\cdot		
\cdot		

Asymptotic stability: $(m_q + k_a) < 0$ and $(m_q k_a - m_a) > 0$

Systems Analysis and Design

- **System Characteristics**
 - Degree or extent of system stability
 - Steady state performance (response doesn't approach zero)
 - Transient performance (response approaches zero when $t \rightarrow \infty$)
- **Analysis Methods**
 - Determine transfer functions for each system components
 - Formulate system model by integrating components (Block Diagram)
 - Determine the system response characteristics (Root-locus, Bode-plot, Nyquist, Nichols)
- **Design Objectives**
 - Meet performance specifications
 - Frequency/Time domain responses
 - Speed of response, relative stability, system accuracy

Frequency Response Function

For system: $\sum_{i=0}^n a_i \frac{d^i y}{dt^n} = \sum_{i=0}^m b_i \frac{d^i u}{dt^n}$ if $u(t) = e^{st}$, where $s = \sigma + j\omega$

then $y(t) = H(s)e^{st}$, where $H(s) = \frac{\left(\sum_{i=0}^m b_i s^i\right)}{\left(\sum_{i=1}^n a_i s^i\right)}$

When the input are sinusoidal functions, i.e., $u(t) = e^{j\omega t} = \cos \omega t + j \sin \omega t$
then $H(j\omega)$ is called the **frequency response function** of the system
where $H(j\omega) = \rho(j\omega)e^{j\phi(j\omega)}$

- Provide a useful characteristics of system frequency response
- Provide natural framework to specify desired system properties
- Examples: design frequency selective filters in communication systems and audio equipment

Frequency Domain Characteristics

- **Bode Plot (JD. Chap. 15)**

- Magnitude versus frequency in log-log scale
- Phase versus log of frequency

$$H(j\omega) = \frac{b(j\omega)}{a(j\omega)} \Rightarrow \log |H(j\omega)| = \log |b(j\omega)| - \log |a(j\omega)|$$

First – Order System: $\dot{y}(t) + ay(t) = u(t)$

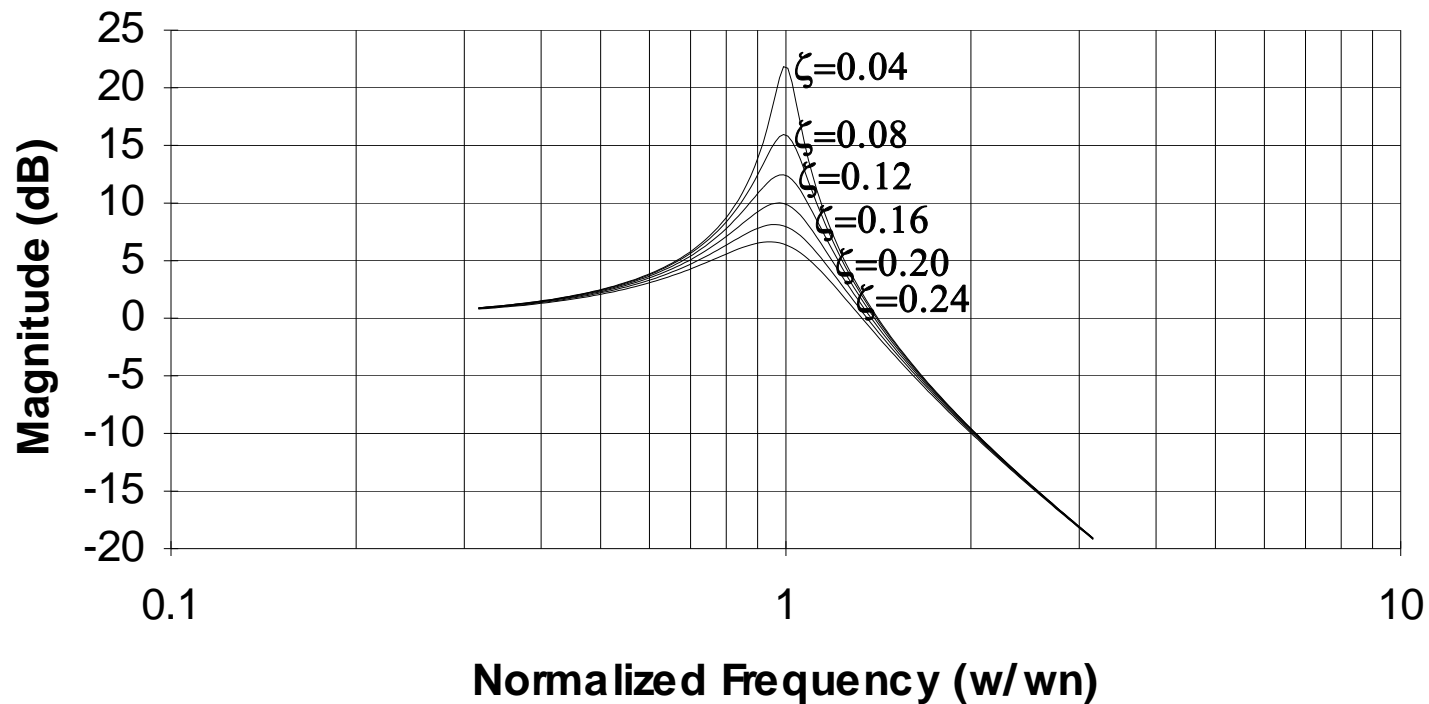
$$H_1(s) = \frac{1}{s + a} \Rightarrow \log |H_1(j\omega)| = -\log a - \log |j(\omega/a) + 1|$$

Second – Order System: $\ddot{y}(t) + a_1\dot{y}(t) + a_2y(t) = u(t)$

$$Ex: H_2(s) = \frac{1}{s^2 + 2\zeta\omega_n s + \omega_n^2} \Rightarrow H_2(j\omega) = \frac{1/\omega_n^2}{(j\omega/\omega_n)^2 + 2\zeta(j\omega/\omega_n) + 1}$$

Bode Plot- second order system

Bode Plots of a Second Order System for Several Damping Values



Time-Domain Characteristics

$\dot{\mathbf{x}}(t) = \mathbf{A}\mathbf{x}(t) + \mathbf{B}\mathbf{u}(t)$ with $\mathbf{u}(t) = \mathbf{1}(t)$ and zero initial condition

Step Response: $\mathbf{x}_s(t) = \int_0^t e^{\mathbf{A}(t-\tau)} \mathbf{B} d\tau = \mathbf{A}^{-1} (e^{\mathbf{A}t} - I) \mathbf{B}$

$\mathbf{x}_s(t) \rightarrow -\mathbf{A}^{-1} \mathbf{B}$ if the system is asymptotically stable

If $\lambda = \lambda_R + j\lambda_I$, then $\tau_A = \max \left| \frac{1}{\text{Re}(\lambda_i)} \right|$ is called the *Time constant* of \mathbf{A}

Ex: $\dot{y}(t) + ay(t) = u(t); \quad y(0) = 0$

step response: $y(t) = \frac{1}{a} (1 - e^{-at}) \mathbf{1}(t), \quad \tau = \frac{1}{a}$

